

# Compact Microstrip Coupled line Bandpass Filter for C Band Applications

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**Abstract**—The paper presents a novel and compact microstrip band pass filter for C-band applications. The filter consists of three parallel-coupled lines quarter wavelength long at the center frequency (6 GHz) of the required operating band (4-8GHz). Quarter wavelength short-circuited stubs in the form of stepped impedance resonators at the end of the central line introduce the required transmission zeros at the upper band edge thus controlling the upper cut off frequency. The width of the coupled lines control the lower cut off frequency.

**Index Terms**— Bandpass filters, Coupled line filters, Microstrip filters, Stepped Impedance Resonator.

## I. INTRODUCTION

The IEEE C-band (4 to 8GHz) and its variations contain frequency ranges that are used for many satellite communications, transmissions, Wi-Fi devices, cordless telephones, and weather radar systems. The rapid growth of mobile and wireless communication system technology in today's world has increased the need for bandpass filters. Due to the advantages of low cost, light weight, small size and easy fabrication, microstrip planar filters have many RF/microwave applications [1, 2]. Parallel-coupled line bandpass filters [4] have been extensively adopted in the RF front end of microwave and wireless communication systems. In this paper a microstrip parallel coupled line filter with shunt short stubs is proposed for C band applications.

Procedure for Paper Submission

## II. FILTER GEOMETRY

The filter consists of three parallel-coupled lines quarter wavelength long ( $L=5.91\text{mm}$ ) at the center frequency (6 GHz) in the required operating band (4-8GHz). The required

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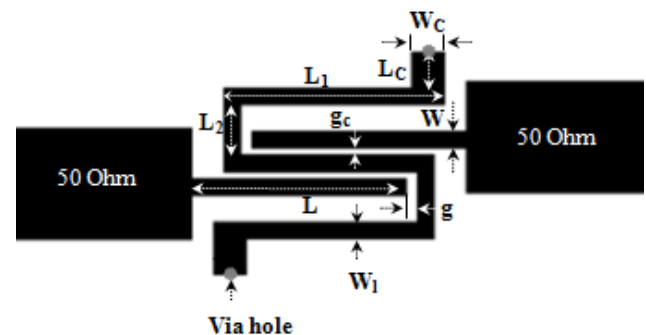
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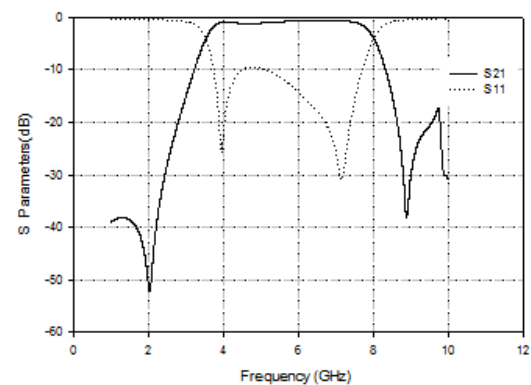
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transmission zeros at the upper end of the pass band are introduced using quarter wavelength short-circuited stubs in the form of stepped impedance resonators (SIR) formed by a high impedance inductive stub and a low impedance capacitive stub ( $L_1$ ,  $L_2$  &  $L_c$ ). The width of the coupled lines ( $W$ ) control the lower cut off frequency. Fig.1 shows the layout of the filter structure designed using a substrate with  $\epsilon_r=4.4$ ,  $h=1.6\text{mm}$  and loss tangent 0.02.

The simulated S parameters are shown in Fig.2. The simulated bandwidth obtained is from 3.51 GHz to 8 GHz. The result shows an insertion loss less than 1 dB and an attenuation of 38.16 dB in the lower stopband and 17.86 dB in the upper stopband. The simulated roll off rate in the lower edge is 32.19dB/GHz and in the upper edge is 49.41 dB/GHz.



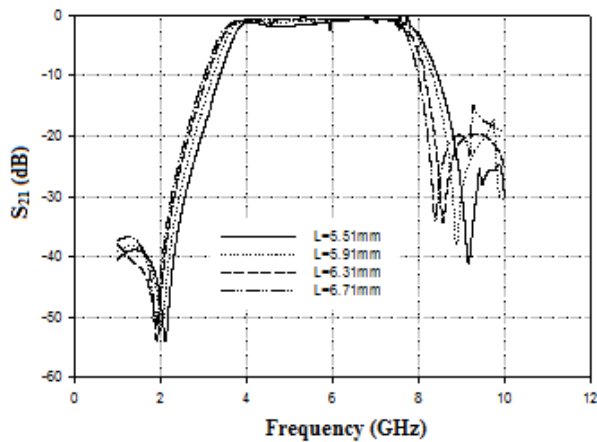
**Fig.1.** Layout of the Filter Structure ( $W_c=0.95$ ,  $W_1=W=0.5$ ,  $L_1=6.2$ ,  $L_2=1.36$ ,  $L_{ind}=L_1+L_2$ ,  $L=5.91$ ,  $g_c=0.15$ ,  $g=0.28$ ,  $L_c=1$ ) All dimensions in mm



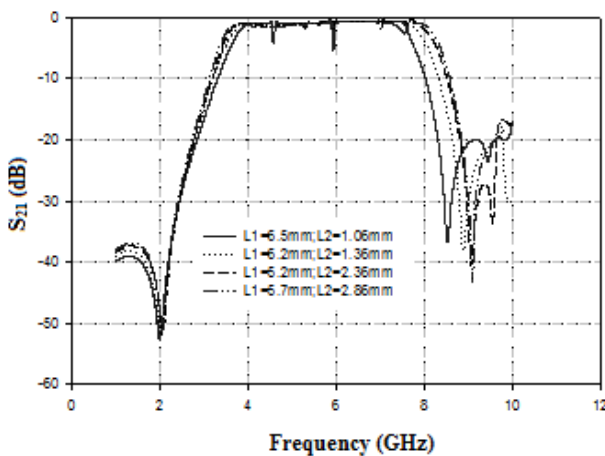
**Fig.2.** Simulated S Parameters

Fig.3 (a) shows the optimetrics study on length of the coupled lines ( $L$ ). The entire band is shifted to right by reducing the length of coupled lines. The optimetrics study on

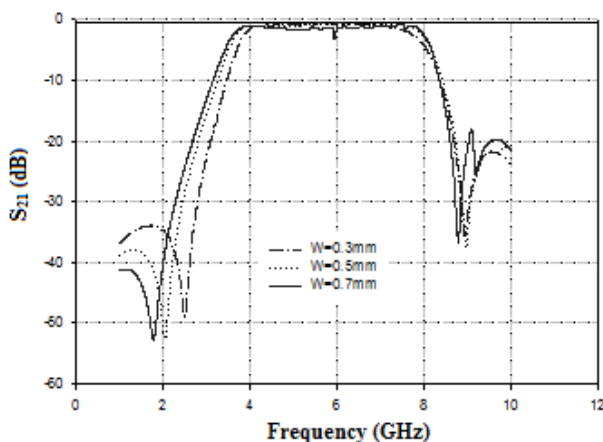
the length of the stub sections without changing the total length is shown in Fig.3 (b). It can be seen from the figure that the upper cut off frequency is increased by reducing the ratio  $L_1:L_2$ . The lower cut off frequency can be varied by varying the width of coupled lines (W) as shown in Fig.3(c).



(a) Entire band is shifted to right by reducing the length of coupled lines



(b) Variation of upper cut-off frequency by changing the length ratio  $L_1:L_2$  by keeping total length of the stub constant



(c) Variation of lower cut-off frequency by changing the width of coupled line

Fig.3. Parametric Analysis

### III. EQUIVALENT CIRCUIT

Fig.4 shows the LC equivalent circuit of the filter modeled using CST Microwave Studio. The values  $L_{SIR}$  and  $C_{SIR}$  represent the parallel LC resonators introduced by the SIR.  $L_3, C_3, L_4, C_4,$  and  $L_5, C_5, L_6, C_6$  represent coupled line sections which give the bandpass nature to the filter.  $C_p$  is the distributed shunt capacitance between transmission line and ground.

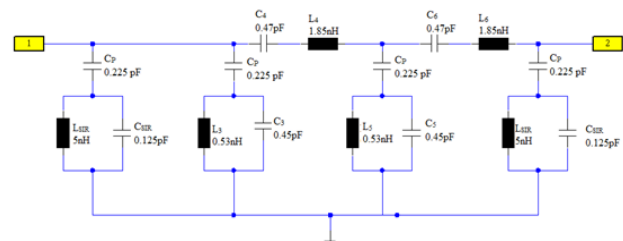


Fig.4. Equivalent circuit of the Filter

The inductance value  $L_{SIR}$  is calculated using the following expression [5].

$$L_i = f_c \lambda_{gl} L / Z_{01} \quad (1)$$

Where,  $L_i = L_1 + L_2 = 7.56$  mm,  $f_c = 6$  GHz,  $\lambda_{gl}$  = guide wavelength for inductive stub = 28.532mm,  $Z_{01} = 113.41$  Ohms is the characteristic impedance of the inductive transmission line section. The computed inductance value is 5nH.

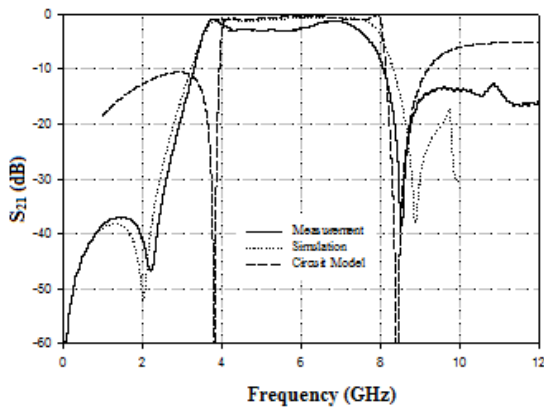
The value of capacitance for the length  $L_c = 1$ mm is computed using the expression [5].

$$L_c = f_c \lambda_{gc} Z_{0c} C_s \quad (2)$$

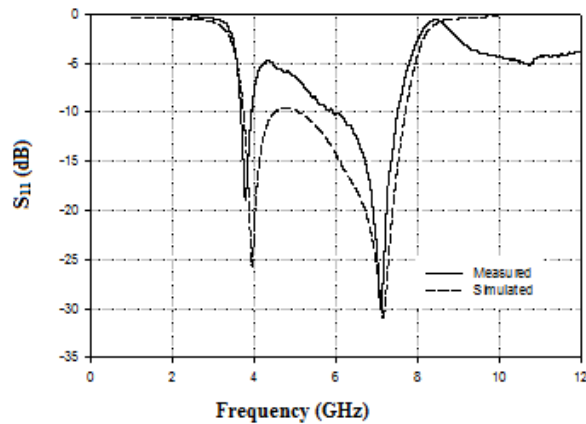
Where,  $f_c = 6$  GHz,  $\lambda_{gc}$  = guide wavelength in the capacitive stub = 28.075 mm,  $Z_{0c} = 90.34$  Ohms is the characteristic impedance of the capacitive transmission line section. The computed capacitance value is 0.625 pF. Taking into consideration the coupling of SIR with other parts of the filter structure, the values are optimised and equivalent circuit with optimised values is shown in Fig.4. The lumped element values corresponding to the coupled line sections ( $L_3-L_6$  and  $C_3-C_6$ ) are computed according to [3].

### IV. EXPERIMENTAL RESULTS

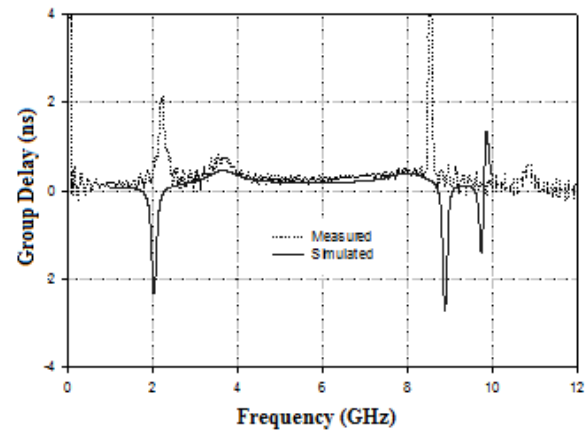
The filter structure is implemented on FR4-epoxy substrate with a dielectric constant of 4.4; thickness 1.6 mm and loss tangent 0.02. Measurements are taken using Agilent E8362B PNA. Experimental results closely agree with simulated results. The simulated and measurement results are shown in Fig.5 (a-c). Measured stop band attenuation is better than 37dB in the lower side and 13dB in the upper side. The photograph of the fabricated prototype filter is shown in Fig.5 (d). Roll off rate is 33.35 dB/GHz in the lower side and 44.58dB/GHz in the upper side. Group delay is 0.25ns and variations are less than 0.15ns. Slight discrepancies in measured results can be attributed to fabrication inaccuracies.



(a)  $S_{21}$  of circuit simulation, EM simulation and measurement for the Proposed filter.



(b) Simulated and Measured  $S_{11}$



(c) Simulated and Measured Group Delay of the proposed filter

Fig.5.Results

Table I. shows the comparative study of parameters of the proposed filter with similar reported works. As can be seen from Table.1 the proposed filter is compact and has better lower stopband attenuation and good roll off rate. The insertion loss can be improved by using a low loss substrate.

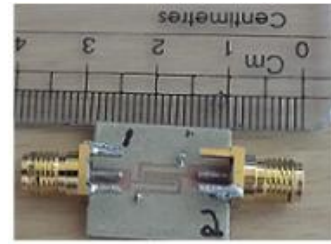


Fig.5. (d) Photograph of the Fabricated Prototype filter

Table I. Comparison of Parameters of Proposed filter with similar works.

Parameter	Proposed filter	[4]	[5]	[6]	[7]	[8]
Insertion Loss(dB)	3.2	1	2.4	1.8	0.53	2.1
Passband(GHz)	3.53-8	3.7-8.3	3.17-10.6	3.1-10.6	3.85-10.44	1.85-3.05
Rolloff Rate – Lower,Upper(dB/GHz)	33.35, 44.58	Not Specified	147, 30	Not Specified	Not Specified	Not Specified
Stopband attenuation- Lower,Upper(dB)	37,13	25,24	28,20	Not Specified	Not Specified	28,18
Group delay variations(nS)	0.25	0.25	0.2	0.2	0.25	Not specified
Size	17.85×6.24 mm <sup>2</sup>	16×3.15 mm <sup>2</sup>	20×6.6 mm <sup>2</sup>	35×8mm <sup>2</sup>	5×7.6mm <sup>2</sup>	22×18 mm <sup>2</sup>
Substrate [ε <sub>r</sub> /h]	4.4/1.6mm	10.8/1.27 mm	4.4/1.6 mm	2.2/0.254 mm	2.2/0.508 mm	Not specified

## V. CONCLUSION

A novel and compact microstrip band pass filter is presented for C-band applications. Good roll off rate and better stopband attenuation are the main features of the proposed filter. The filter exhibits good group delay performance making it suitable for communication applications. Use of a low loss substrate can lead to lesser insertion loss.

## ACKNOWLEDGMENT

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